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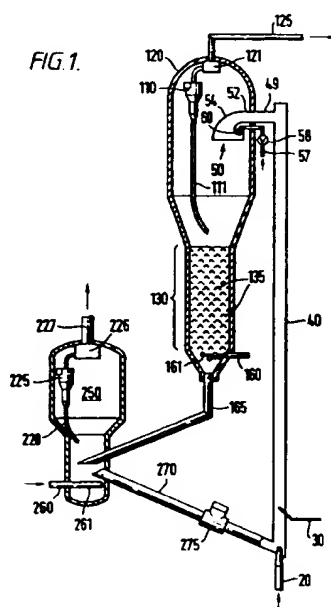
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(54) **FCC Riser discharge separation and quench.**

(57) In a fluid catalytic cracking (FCC) process the reaction mixture from a riser reactor (40) is rapidly separated by separator (50) into a predominantly spent catalyst phase and a predominantly cracked hydrocarbon phase. The separated hydrocarbon is immediately quenched to an unreactive temperature by quench fluid from a nozzle (60), the nozzle discharging all the quench fluid into the separated hydrocarbon but not into the separated spent catalyst. An increase in debutanized naphtha yield can be achieved. By avoiding catalyst quenching, heat duty is saved in the catalyst regenerator (250).



The invention is a process and apparatus for the separation of a catalyst phase from a cracked hydrocarbon phase in the fluid catalyst cracking (FCC) of hydrocarbon. More particularly, the invention is a process and apparatus to reduce post riser cracking of cracked hydrocarbon discharged from a riser reactor. The invention is also a process and apparatus which heat integrates the riser reactor, and the catalyst regenerator, thereby reducing the heat duty in a fluid catalyst cracking (FCC) process.

Fluid catalytic cracking (FCC) processes are known in the art. State of the art commercial catalytic cracking catalysts for these processes are highly active and selective for converting hydrocarbon charge stocks to liquid fuel products. With such active catalysts it is preferable to conduct catalytic cracking reactions in a dilute phase transport type reaction system with a relatively short period of contact between the catalyst and the hydrocarbon feedstock, e.g. 0.2 to 10 seconds.

The control of short contact times, optimum for state of the art catalysts in dense phase fluidized bed reactors is not feasible. Consequently, catalytic cracking systems have been developed in which the primary cracking reaction is carried out in a transfer line reactor or riser reactor. In such systems, the catalyst is dispersed in the hydrocarbon feedstock and passed through an elongated reaction zone at relatively high velocity. In these transfer line reactor systems, feedstock acts as a carrier for the catalyst. In a typical upflow riser reactor, the hydrocarbon vapors move with sufficient velocity as to maintain the catalyst particles in suspension with a minimum of back mixing of the catalyst particles with the gaseous carrier. Thus development of improved fluid catalytic cracking catalysts has led to the development and utilization of reactors in which the reaction is carried out with the solid catalysts particles in a relatively dilute phase with the catalyst dispersed or suspended in hydrocarbon vapors undergoing reaction, e.g., cracking.

The cracking reactions are conveniently carried out in high velocity transport line reactors wherein the catalyst is moved from one vessel to another by the hydrocarbon vapors. Such reactors have become known in the art as risers or riser reactors. The catalyst and hydrocarbon mixture passes from the transfer line reactor into a first separation zone in which hydrocarbon vapors are separated from the catalyst. The catalyst particles are then passed into a second separation zone, usually a dense fluidized bed stripping zone wherein further separation of hydrocarbons from the catalyst takes place by stripping the catalyst with steam. After separation of hydrocarbons from the catalyst, the catalyst is introduced into a regeneration zone where carbonaceous residues are removed by burning with air or other oxygen-containing gas. After regeneration, hot catalyst from the regeneration zone is reintroduced into the transfer line reactor with fresh hydrocarbon feed.

As stated, state of the art catalytic cracking catalysts are highly active. With the introduction of these highly active catalysts the first separation zone has become a limiting unit operation. When catalyst is not rapidly separated from vapor and the vapor quenched once the desired reactions have taken place, the cracking reactions will continue with the production of less desirable products. Rough-cut cyclones have been used as a first separation stage between catalyst and vapor, followed by finer cut cyclones to remove fines from the vapor.

U.S. Patent 4,664,888 to L. F. Castagnos, Jr. teaches a rough cut catalyst-vapor separator in a fluid catalytic cracking process. In the separator a separator surface causes the oil-catalyst mixture to undergo a 180° turn. Catalyst moves toward the separator surface to form a catalytic phase. Vapor is squeezed away from the wall forming a vapor phase. A shave edge maintains the separation.

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Perry's Chemical Engineers' Handbook, 4th Ed., p. 18-64 teaches fan nozzles. The nozzles form a flat fan-shaped fluid sheet. The included angle of the fan is from 10 deg. to 130 deg. in standard nozzles and capacities range from 0.38 to 75.7 litres/minute (0.1 to 20 gal./minute).

The invention is an improvement in a fluid catalytic cracking (FCC) process. In an FCC process, a hydrocarbon feedstock in suspension with a fluidized catalyst is cracked at catalytic reaction temperature to form a mixture of cracked hydrocarbon and spent catalyst. The mixture is separated into separated cracked hydrocarbon and spent catalyst phases.

The improvement comprises quenching the separated cracked hydrocarbon to an unreactive temperature substantially simultaneously with separating the two phases. The quenching of the separated cracked hydrocarbon is carried out in the absence of quenching spent catalyst. The absence of quenching spent catalyst results in a reduction in heat duty in the catalyst regenerator where carbonaceous matter is burned from the catalyst.

Fig. 1 is a diagrammatic arrangement of a fluid catalytic cracking process comprising a riser reactor, catalyst separator, reactor vessel and catalyst regenerator.

Fig. 2 is a schematic side view of a separator/quench apparatus.

Fig. 3A is an end elevation of a fan nozzle.

5 Fig. 3B is a longitudinal section through a fan nozzle showing a first spray configuration.

Fig. 3C is a longitudinal section through a fan nozzle showing a second spray configuration.

Reference is made to Fig. 1 which is representative of an apparatus for contacting a hydrocarbon feedstock with finely divided fluidized catalyst in riser reactor 40 at catalytic cracking conditions. A clean, freshly regenerated catalyst is delivered from regenerated catalyst standpipe 270 into the lower portion of
 10 riser reactor 40. The regenerated catalyst has a carbon content less than about 0.1 wt% and an ASTM microactivity of 60 to 70. As the catalyst enters the riser, its temperature decreases from 760°C to 700°C by the addition of a fluidization medium delivered by line 20. The fluidization medium may be steam, nitrogen or low molecular weight hydrocarbons such as methane, ethane, ethylene or fuel gas. The amount of fluidization medium must be sufficient to fluidize the fluid zeolite catalyst in the base of riser 40 above
 15 the minimum fluidization velocity to move the catalyst toward the injection point of the hydrocarbon oil. A liquid feedstock, such as vacuum gas oil, atmospheric residuum, deasphalted oil or combinations thereof, having a boiling range of about 200°C to 540°C, is heated and delivered to riser reactor 40 through conduit 30. The feedstock enters the riser by way of an injection nozzle (not shown) which may be a single nozzle or an arrangement of more than one nozzle which mixes oil and catalyst quickly and completely after
 20 injection. The amount of catalyst circulated must be enough to completely vaporize the oil and be sufficient to crack the feedstock to a slate of products which when corrected to room temperature include gases, low boiling liquids and fuel boiling range liquids such as gasoline and light cycle gas oil. The mixture of products and unconverted gas oil vapor have sufficient velocity to transport the fluid catalyst upwardly through the riser 40.

25 The riser conversion zone comprises the internal volume of the riser from the lower injection point to separator/quencher 50 including transitional conduit 49 and discharge conduit 52. Separator/quencher 50 is close coupled with riser 40 so that all of the reaction mixture from the riser reactor flows into it. Separated hydrocarbon vapor passes into reactor vessel 120. From there, hydrocarbon vapor passes into secondary cyclone 110, plenum 121 and is transported through conduit 125 to fractionation and purification means (not shown). Separated catalyst from separator/quencher 50 and catalyst from secondary cyclone 110 falls to a
 30 lower portion of the reactor vessel 120 through dipleg 111. The dipleg is sealed by means such as J-valves, trickle valves, flapper valves (not shown).

The catalyst flows into the stripping zone 130 containing baffles 135 or other means to contact the catalyst and stripping gas. The stripping gas may be nitrogen, steam or other suitable material delivered by
 35 conduit 160 to distributor 161. Distributor 161 uniformly disperses the stripping gas into the stripping zone 130 and removes volatile and volatilizable hydrocarbons. A hotter catalyst temperature in stripping zone 30 increases the amount of hydrocarbon volatilized and stripped from the catalyst. The hydrocarbons stripped from the catalyst and stripping gas flow out of reactor vessel 120 with the product vapors through secondary cyclone separator 110, plenum 121 and conduit 125.

40 The stripped catalyst leaves stripping zone 130 and is delivered to the regenerator 250 by way of spent catalyst standpipe 165. The regenerator 250 contains a lower dense phase bed of catalyst and an upper dilute phase of catalyst. Catalyst is uniformly distributed across the upper surface of the dense phase bed. Most of the coke is removed in the dense phase bed. A combustion medium of air or oxygen and nitrogen is delivered by conduit 260 to a distribution device 261 to mix combustion medium and coked catalyst.
 45 Coke is burned from the catalyst to give a flue gas containing amounts of CO₂, SO₂, and NO_x. The combustion of the coke to CO₂ is preferably carried out at a regenerator temperature above about 650°C and below about 760°C in the presence of a combustion promoter such as platinum residing on the catalyst so that 0.1 wt% or less residual carbon is left on the catalyst. The flue gas passes through the regenerator dilute phase, cyclone 225, plenum 226 and flue gas line 227 for further processing. As the flue
 50 gas passes through the cyclone, catalyst is separated and returned to the dense bed by way of dipleg 228. The regenerated catalyst flows from the dense bed to standpipe 270. Slide valve 275 regulates the flow of regenerated catalyst from standpipe 270 to riser 40.

Reference is made to Fig. 2, a schematic representation of separator/quencher 50.

55 A catalyst and cracked hydrocarbon mixture flows through discharge conduit 52 which directs the mixture toward centrifugal separator wall 54. Centrifugal separator wall 54 is geometrically described by one-quarter of a circle in the vertical plane parallel to the surface of the paper. The radius of the circle is substantially larger than the radius of discharge conduit 52. The center of the circle is point 55. In this representation, the radius is approximately five times the radius of discharge conduit 52. This relatively

large axis of rotation causes a deflection of the mixture from flow in the horizontal direction to downward flow. This change in direction also causes the centrifugal disengagement or separation of the stream into a downwardly flowing predominantly catalyst phase which is in contact with wall 54 and a predominantly cracked vapor phase, spaced from the wall 54.

Quench fluid is introduced via quench line 57 and valve 58 into separator/quencher 50. The quench fluid is discharged into the predominately cracked vapor phase by means of nozzle 60.

Figs. 3A, 3B and 3C are three views of nozzle 60 and the spray pattern of quench fluid it produces in separator/quencher 50. The spray pattern is critical to the invention. Substantially all of the quench fluid spray must remain in the cracked vapor phase and not cross into the catalyst phase before the quench fluid is vaporized. Nozzles which produce such a spray pattern are commercially available. Fish tail nozzles and fan nozzles produce a relatively flat sheet or flat ellipse of spray which is well defined. The spray is so well defined that the nozzle is selected for the exact spray angle in both dimensions.

A fan nozzle produces a flat sheet of spray in an elliptical spray pattern. The sheet becomes thinner with distance from the nozzle. Surface tension causes the thin sheets to break up into droplets at a distance from the nozzle.

Fan nozzles which produce spray angles of 10° to 110° are commercially available. It is characteristic of fan nozzles that sheets of very uniform thickness are formed at included angles of 50° to 10° . At larger included angles two separate streams called horns are produced with liquid sheets connecting the horns. These horns have much less surface area than the sheets and may remain in the liquid state long enough to contact hot catalyst, which is undesirable because of quenching.

The nozzles which produce more uniform sheets of quench fluid also produce the narrow pattern required to avoid impingement of the catalyst phase with quench fluid. The fan nozzle is therefore oriented so that the long axis of the ellipse is perpendicular to the cracked hydrocarbon-catalyst interface. The short axis is perpendicular with the interface. The long axis has an included angle 62 of 50° in Fig. 3B. The short axis has an included angle 64 of 10° in Fig. 3C.

When hydrocarbon fractions are catalytically cracked, the most desirable products are debutanized naphtha with an end point about 220°C (gasoline) and light cycle gas oil boiling from 220°C to about 355°C . The highest yield of these fractions is achieved by cracking at fluid catalytic cracking conditions at a temperature in the range 480°C to 590°C , preferably 510°C to 540°C for 0.5 to 1.5 seconds and then terminating the cracking reaction at the riser outlet. The cracking reaction is terminated at temperatures of about 500°C and less defined herein as an unreactive temperature. When the cracking reaction continues for even short periods of time past the optimum, the yield of the most desirable products decreases. The decrease in desirable products is attributed to an increase in the dry (hydrocarbon) gas make.

Attempts have been made to improve the separation of catalyst and hydrocarbon product in order to stop the catalytic cracking reaction. The yield of desirable products has been increased, but these are increments of yield to be gained by terminating thermal cracking reactions as well as catalytic cracking reactions.

Methods of quenching riser reactor effluent have included quenching the entire hydrocarbon-catalyst mixture. The portion of the quench which is used on the catalyst must be made up in the regenerator. Therefore the heat to quench the catalyst is lost to the catalyst regeneration stage and the same amount of heat must be added to the catalyst regenerator. To make up this heat, torch oil is added directly to the catalyst regenerator to raise the regenerator to the desired regeneration temperature. This torch oil can be reduced or even eliminated if the quenching of catalyst is avoided.

This invention is shown by way of example.

EXAMPLE

A computer simulation of a commercial fluid catalytic cracking unit such as that shown in Fig. 1 was made based on correlations of operating data taken from a commercial process. Two simulation runs are reported in Table 1. Run 1 gives the product yields and conversion from the rapid separation of hydrocarbon product from catalyst in the absence of quench. Run 2 gives the product yields and conversion when the hydrocarbon product was rapidly separated from catalyst and then quenched. Quenching in Run 2 yielded the same amount of total gas to the compressor as Run 1 but less total dry gas. This allowed for an increased feed rate in Run 2 at constant gas compressor loading (total gas to compressor).

The data shows that the conversion of feedstock decreased while the yield of debutanized naphtha (DB naph) increased with quenching. This is attributed to the reduction in overcracking.

TABLE 1

	Run 1 (Comparative)	Run 2
<u>Fresh Feed</u>		
API Gravity	19°	19°
Sulfur	1.71 Wt%	1.71 Wt%
Carbon Residue	0.25 Wt%	0.25 Wt%
<u>Operating Conditions</u>		
Fresh Feed Rate	29400 B/D	32600 B/D
Throughput Ratio	1.07	1.07
Feed Preheat	250°C	250°C
Riser Outlet	529°C	529°C
Amount of Quench	0°C	28°C
Regenerator Bed	733°C	723°C
Conversion 430°F	73.55 Vol%	72.34 Vol%

1 B/D (barrel per day) = 159 litres per day

		Run 1 (Comparative)		Run 2	
	<u>Yields: Perfect Fractionation</u>	<u>Vol%</u>	<u>Wt%</u>	<u>Vol%</u>	<u>Wt%</u>
5	H ₂ S		0.80		0.81
	H ₂		0.09		0.09
10	C1		1.69		1.34
	C2		1.55		1.24
	C2 Olefin		1.20		0.97
15	Total Dry Gas H ₂ -C ₂ Olefin		4.53		3.64
	C3	2.49	1.34	2.38	1.28
	C3 Olefin	7.81	4.32	7.50	4.15
20	iC4	2.97	1.78	2.76	1.65
	nC4	1.56	0.97	1.50	0.93
	C4 Olefin	7.49	4.83	7.20	4.64
25	Total C3-C4	22.32	13.24	21.34	12.65
	Total C3-C4 Olefins	15.30	9.15	14.70	8.79
30	Total Gas to Compressor H ₂ S-C4 Olefin Lb-Mol/hr		2,161		2,164
	Lt. Naph	37.32	27.20	37.77	27.53
35	Hvy. Naph	22.35	19.77	22.61	20.00
	DB Naph	59.67	46.97	60.38	47.53
	LCGO	17.87	18.54	19.57	20.26
40	HCGO	8.58	10.53	8.09	9.84
	Coke		5.39		5.27
	DB Naph RON		93.7		93.4
45	Octane- bbl/hr		68,491		76,603

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Carbon Residue -	Conradson Carbon Residue ASTM D-4530-85	
5 DB Naph	-	debutanized naphtha C5- 221°C
Lt. Naph	-	light naphtha C5- 121°C
Hvy. Naph	-	heavy naphtha 121°C - 221°C
10 LCGO	-	light cycle gas oil 221°C - 343°C
HCGO	-	heavy cycle gas oil 343°C - 565°C
RON	-	research octane number
15 B/D	-	barrels/day (1 B/D = 159 litres/day)

While particular embodiments of the invention have been described, it will be understood that the invention is not limited thereto since modifications may be made and it is therefore contemplated to cover by the appended claims any such modifications as fall within the spirit and scope of the claims.

Claims

- 25 1. A fluid catalytic cracking process comprising:
 - cracking a hydrocarbon feedstock in suspension with a fluidized catalyst at a catalytic reaction temperature to form a mixture of cracked hydrocarbon and spent catalyst; and
 - separating said mixture into predominantly cracked hydrocarbon and predominantly spent catalyst; characterized by:
 - 30 substantially simultaneously with separating said mixture, quenching said separated cracked hydrocarbon to an unreactive temperature, but not quenching said separated spent catalyst.
2. A process according to claim 1 characterized by regenerating said spent catalyst at a regeneration temperature above said catalytic reaction temperature to yield regenerated catalyst, and passing said regenerated catalyst for use in said cracking step.
- 35 3. A process according to claim 2 characterized in that said regeneration temperature is in the range of substantially 650°C to 760°C.
- 40 4. A process according to any one of claims 1 to 3 characterized in that said quenching step does not precede said separating step.
5. A process according to any one of claims 1 to 4 characterized in that said catalytic reaction temperature is in the range of substantially 510°C to 540°C.
- 45 6. A process according to any one of claims 1 to 5 characterized in that said unreactive temperature is at least 22°C below said catalytic reaction temperature.
7. A process according to claim 6 characterized in that said unreactive temperature is about 22°C to 28°C below said catalytic reaction temperature.
- 50 8. Apparatus for the fluid catalytic cracking of a hydrocarbon feedstock comprising:
 - a riser conversion zone defined by a vertically elongate tubular conduit (40) having a lower upstream end (30) and an upper downstream end (49), said downstream end terminating within a reactor vessel (120);
 - 55 means (20,30) for providing a suspension of hydrocarbon feedstock and catalyst at the upstream end (30) of said riser conversion zone to produce a mixture of spent catalyst and cracked hydrocarbon discharging from the downstream end (49) of said riser conversion zone; and

a first conduit (52) directly connecting the downstream end (49) of said riser conversion zone to a separator (50);

characterized in that:

said separator (50) comprises:

- 5 a separation surface (54) curved and positioned to cause said mixture to flow therealong thereby centrifugally separating said mixture into a predominantly spent catalytic phase in contact with the separation surface (54) and a predominantly cracked hydrocarbon phase spaced from said surface; and
- 10 a second conduit (57) for providing a quench fluid to a nozzle (60) having a discharge pattern causing discharge of substantially all of said quench fluid into said separated cracked hydrocarbon phase.
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- 50
- 55

FIG. 1.

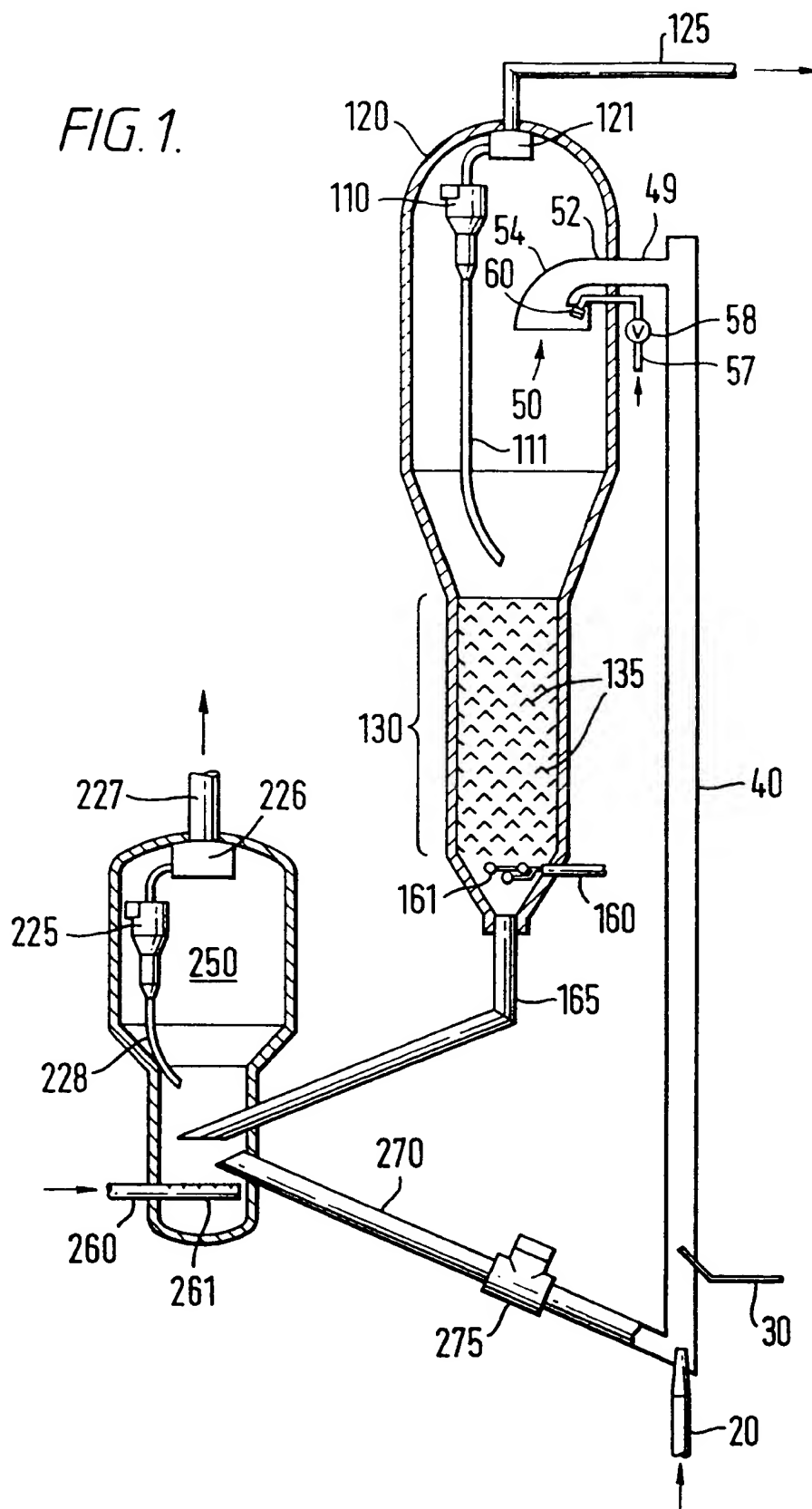


FIG. 2.

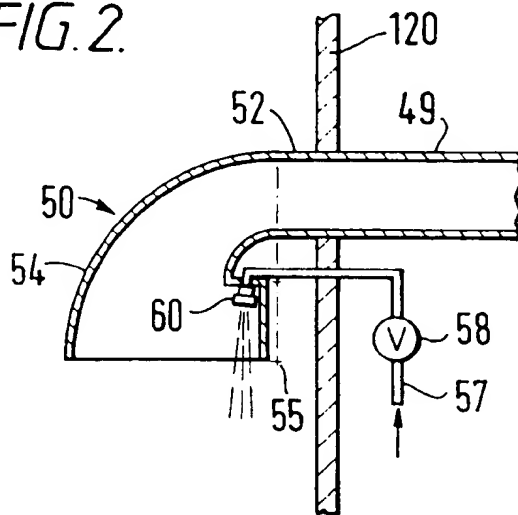


FIG. 3A

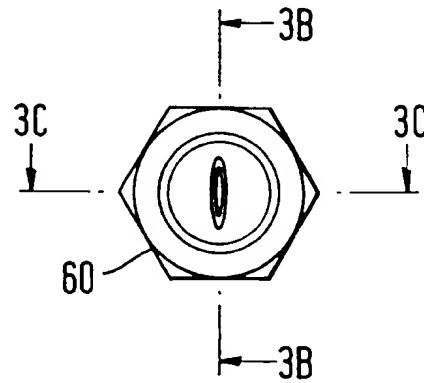


FIG. 3B

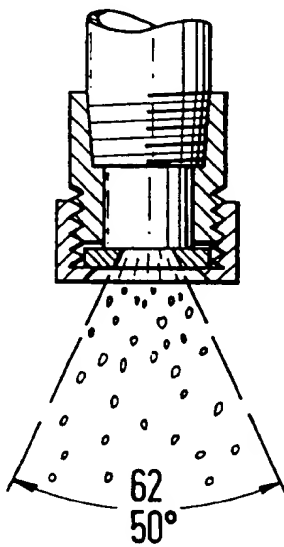
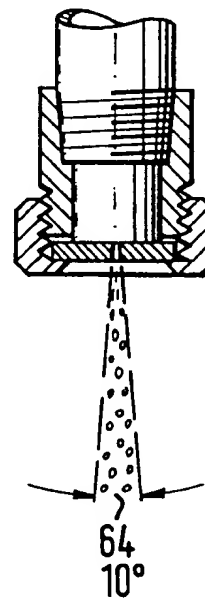


FIG. 3C





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EUROPEAN SEARCH REPORT

Application Number

EP 92 30 9525

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
X	EP-A-0 448 860 (AMOCO) * the whole document *	1-7	C10G11/18
X	US-A-5 073 249 (MOBIL OIL) * the whole document *	1-7	
D,A	US-A-4 764 268 (TEXACO) -----		
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			C10G
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 09 JUNE 1993	Examiner MICHIELS P.
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure F : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ----- & : member of the same patent family, corresponding document	

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Trennung und Abschreckung eines Abflusses einem FCC-Steigrohr

Séparation et trempe d'une décharge d'un tuyau montant d'un système FCC

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(56) References cited:
EP-A- 0 448 860 **US-A- 4 764 268**
US-A- 5 073 249

EP 0 593 823 B1

Note: Within nine months from the publication of the mention of the grant of the European patent, any person may give notice to the European Patent Office of opposition to the European patent granted. Notice of opposition shall be filed in a written reasoned statement. It shall not be deemed to have been filed until the opposition fee has been paid. (Art. 99(1) European Patent Convention).

Description

The invention is a process and apparatus for the separation of a catalyst phase from a cracked hydrocarbon phase in the fluid catalyst cracking (FCC) of hydrocarbon. More particularly the invention is a process and apparatus to reduce post riser cracking of cracked hydrocarbon discharged from a riser reactor. The invention is also a process and apparatus which heat integrates the riser reactor, and the catalyst regenerator, thereby reducing the heat duty in a fluid catalyst cracking (FCC) process.

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The cracking reactions are conveniently carried out in high velocity transport line reactors wherein the catalyst is moved from one vessel to another by the hydrocarbon vapors. Such reactors have become known in the art as risers or riser reactors. The catalyst and hydrocarbon mixture passes from the transfer line reactor into a first separation zone in which hydrocarbon vapors are separated from the catalyst. The catalyst particles are then passed into a second separation zone, usually a dense fluidized bed stripping zone wherein further separation of hydrocarbons from the catalyst takes place by stripping the catalyst with steam. After separation of hydrocarbons from the catalyst, the catalyst is introduced into a regeneration zone where carbonaceous residues are removed by burning with air or other oxygen-containing gas. After regeneration, hot catalyst from the regeneration zone is reintroduced into the transfer line reactor with fresh hydrocarbon feed.

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Fig. 3B is a longitudinal section through a fan nozzle showing a first spray configuration

Fig. 3C is a longitudinal section through a fan nozzle showing a second spray configuration.

Reference is made to Fig. 1 which is representative of an apparatus for contacting a hydrocarbon feedstock with finely divided fluidized catalyst in riser reactor 40 at catalytic cracking conditions. A clean, freshly regenerated catalyst is delivered from regenerated catalyst standpipe 270 into the lower portion of riser reactor 40. The regenerated catalyst has a carbon content less than about 0.1 wt% and an ASTM microactivity of 60 to 70. As the catalyst enters the riser, its temperature decreases from 760°C to 700°C by the addition of a fluidization medium delivered by line 20. The fluidization medium may be steam, nitrogen or low molecular weight hydrocarbons such as methane, ethane, ethylene or fuel gas. The amount of fluidization medium must be sufficient to fluidize the fluid zeolite catalyst in the base of riser 40 above the minimum fluidization velocity to move the catalyst toward the injection point of the hydrocarbon oil. A liquid feedstock, such as vacuum gas oil, atmospheric residuum, deasphalted oil or combinations thereof, having a boiling range of about 200°C to 540°C, is heated and delivered to riser reactor 40 through conduit 30. The feedstock enters the riser by way of an injection nozzle (not shown) which may be a single nozzle or an arrangement of more than one nozzle which mixes oil and catalyst quickly and completely after injection. The amount of catalyst circulated must be enough to completely vaporize the oil and be sufficient to crack the feedstock to a slate of products which when corrected to room temperature include gases, low boiling liquids and fuel boiling range liquids such as gasoline and light cycle gas oil. The mixture of products and unconverted gas oil vapor have sufficient velocity to transport the fluid catalyst upwardly through the riser 40.

The riser conversion zone comprises the internal volume of the riser from the lower injection point to separator/quencher 50 including transitional conduit 49 and discharge conduit 52. Separator/quencher 50 is close coupled with riser 40 so that all of the reaction mixture from the riser reactor flows into it. Separated hydrocarbon vapor passes into reactor vessel 120. From there, hydrocarbon vapor passes into secondary cyclone 110, plenum 121 and is transported through conduit 125 to fractionation and purification means (not shown). Separated catalyst from separator/quencher 50 and catalyst from secondary cyclone 110 falls to a lower portion of the reactor vessel 120 through dipleg 111. The dipleg is sealed by means such as J-valves, trickle valves, flapper valves (not shown).

The catalyst flows into the stripping zone 130 containing baffles 135 or other means to contact the catalyst and stripping gas. The stripping gas may be nitrogen, steam or other suitable material delivered by conduit 160 to distributor 161. Distributor 161 uniformly disperses the stripping gas into the stripping zone 130 and removes volatile and volatilizable hydrocarbons. A hotter catalyst temperature in stripping zone 30 increases the amount of hydrocarbon volatilized and stripped from the catalyst. The hydrocarbons stripped from the catalyst and stripping gas flow out of reactor vessel 120 with the product vapors through secondary cyclone separator 110, plenum 121 and conduit 125.

The stripped catalyst leaves stripping zone 130 and is delivered to the regenerator 250 by way of spent catalyst standpipe 165. The regenerator 250 contains a lower dense phase bed of catalyst and an upper dilute phase of catalyst. Catalyst is uniformly distributed across the upper surface of the dense phase bed. Most of the coke is removed in the dense phase bed. A combustion medium of air or oxygen and nitrogen is delivered by conduit 260 to a distribution device 261 to mix combustion medium and coked catalyst. Coke is burned from the catalyst to give a flue gas containing amounts of CO₂, SO₂, and NO_x. The combustion of the coke to CO₂ is preferably carried out at a regenerator temperature above about 650°C and below about 760°C in the presence of a combustion promoter such as platinum residing on the catalyst so that 0.1 wt% or less residual carbon is left on the catalyst. The flue gas passes through the regenerator dilute phase, cyclone 225, plenum 226 and flue gas line 227 for further processing. As the flue gas passes through the cyclone, catalyst is separated and returned to the dense bed by way of dipleg 228. The regenerated catalyst flows from the dense bed to standpipe 270. Slide valve 275 regulates the flow of regenerated catalyst from standpipe 270 to riser 40.

Reference is made to Fig. 2, a schematic representation of separator/quencher 50.

A catalyst and cracked hydrocarbon mixture flows through discharge conduit 52 which directs the mixture toward centrifugal separator wall 54. Centrifugal separator wall 54 is geometrically described by one-quarter of a circle in the vertical plane parallel to the surface of the paper. The radius of the circle is substantially larger than the radius of discharge conduit 52. The center of the circle is point 55. In this representation, the radius is approximately five times the radius of discharge conduit 52. This relatively large axis of rotation causes a deflection of the mixture from flow in the horizontal direction to downward flow. This change in direction also causes the centrifugal disengagement or separation of the stream into a downwardly flowing predominantly catalyst phase which is in contact with wall 54 and a predominantly cracked vapor phase, spaced from the wall 54.

Quench fluid is introduced via quench line 57 and valve 58 into separator/quencher 50. The quench fluid is discharged into the predominately cracked vapor phase by means of nozzle 60.

Figs. 3A, 3B and 3C are three views of nozzle 60 and the spray pattern of quench fluid it produces in separator/quencher 50. The spray pattern is critical to the invention. Substantially all of the quench fluid spray must remain in the cracked vapor phase and not cross into the catalyst phase before the quench fluid is vaporized. Nozzles which produce such a spray pattern are commercially available. Fish tail nozzles and fan nozzles produce a relatively flat

sheet or flat ellipse of spray which is well defined. The spray is so well defined that the nozzle is selected for the exact spray angle in both dimensions.

A fan nozzle produces a flat sheet of spray in an elliptical spray pattern. The sheet becomes thinner with distance from the nozzle. Surface tension causes the thin sheets to break up into droplets at a distance from the nozzle.

Fan nozzles which produce spray angles of 10° to 110° are commercially available. It is characteristic of fan nozzles that sheets of very uniform thickness are formed at included angles of 50° to 10°. At larger included angles two separate streams called horns are produced with liquid sheets connecting the horns. These horns have much less surface area than the sheets and may remain in the liquid state long enough to contact hot catalyst, which is undesirable because of quenching.

The nozzles which produce more uniform sheets of quench fluid also produce the narrow pattern required to avoid impingement of the catalyst phase with quench fluid. The fan nozzle is therefore oriented so that the long axis of the ellipse is perpendicular to the cracked hydrocarbon-catalyst interface. The short axis is perpendicular with the interface. The long axis has an included angle of 50° in Fig. 3B. The short axis has an included angle of 10° in Fig. 3C.

When hydrocarbon fractions are catalytically cracked, the most desirable products are debutanized naphtha with an end point about 220°C (gasoline) and light cycle gas oil boiling from 220°C to about 355°C. The highest yield of these fractions is achieved by cracking at fluid catalytic cracking conditions at a temperature in the range 480°C to 590°C, preferably 510°C to 540°C for 0.5 to 1.5 seconds and then terminating the cracking reaction at the riser outlet. The cracking reaction is terminated at temperatures of about 500°C and less defined herein as an unreactive temperature. When the cracking reaction continues for even short periods of time past the optimum, the yield of the most desirable products decreases. The decrease in desirable products is attributed to an increase in the dry (hydrocarbon) gas make.

Attempts have been made to improve the separation of catalyst and hydrocarbon product in order to stop the catalytic cracking reaction. The yield of desirable products has been increased, but these are increments of yield to be gained by terminating thermal cracking reactions as well as catalytic cracking reactions.

Methods of quenching riser reactor effluent have included quenching the entire hydrocarbon-catalyst mixture. The portion of the quench which is used on the catalyst must be made up in the regenerator. Therefore the heat to quench the catalyst is lost to the catalyst regeneration stage and the same amount of heat must be added to the catalyst regenerator. To make up this heat, torch oil is added directly to the catalyst regenerator to raise the regenerator to the desired regeneration temperature. This torch oil can be reduced or even eliminated if the quenching of catalyst is avoided.

This invention is shown by way of example.

EXAMPLE

A computer simulation of a commercial fluid catalytic cracking unit such as that shown in Fig. 1 was made based on correlations of operating data taken from a commercial process. Two simulation runs are reported in Table 1. Run 1 gives the product yields and conversion from the rapid separation of hydrocarbon product from catalyst in the absence of quench. Run 2 gives the product yields and conversion when the hydrocarbon product was rapidly separated from catalyst and then quenched. Quenching in Run 2 yielded the same amount of total gas to the compressor as Run 1 but less total dry gas. This allowed for an increased feed rate in Run 2 at constant gas compressor loading (total gas to compressor).

The data shows that the conversion of feedstock decreased while the yield of debutanized naphtha (DB naph) increased with quenching. This is attributed to the reduction in overcracking.

TABLE 1

	Run 1 (Comparative)	Run 2
Fresh Feed		
API Gravity	19°	19°
Sulfur	1.71 Wt%	1.71 Wt%
Carbon Residue	0.25 Wt%	0.25 Wt%
Operating Conditions		
Fresh Feed Rate	29400 B/D	32600 B/D
Throughput Ratio	1.07	1.07
Feed Preheat	250°C	250°C

TABLE 1 (continued)

	Run 1 (Comparative)	Run 2
Operating Conditions		
Riser Outlet	529°C	529°C
Amount of Quench	0°C	28°C
Regenerator Bed	733°C	723°C
Conversion 430°F	73.55 Vol%	72.34 Vol%
1 B/D (barrel per day) 159 litres per day		

	Run 1 (Comparative)		Run 2	
Yields: Perfect Fractionation	Vol%	Wt%	Vol%	Wt%
H ₂ S		0.80		0.81
H ₂		0.09		0.09
C1		1.69		1.34
C2		1.55		1.24
C2 Olefin		1.20		0.97
Total Dry Gas H ₂ -C ₂ Olefin		4.53		3.64
C3	2.49	1.34	2.38	1.28
C3 Olefin	7.81	4.32	7.50	4.15
iC4	2.97	1.78	2.76	1.65
nC4	1.56	0.97	1.50	0.93
C4 Olefin	7.49	4.83	7.20	4.64
Total C3-C4	22.32	13.24	21.34	12.65
Total C3-C4 Olefins	15.30	9.15	14.70	8.79
Total Gas to Compressor H ₂ S-C4 Olefin Lb-Mol/hr		2,161		2,164
Lt. Naph	37.32	27.20	37.77	27.53
Hvy. Naph	22.35	19.77	22.61	20.00
DB Naph	59.67	46.97	60.38	47.53
LCGO	17.87	18.54	19.57	20.26
HCGO	8.58	10.53	8.09	9.84
Coke		5.39		5.27
DB Naph RON		93.7		93.4
Octane-bbl/hr		68,491		76,603

Carbon Residue -	Conradson Carbon Residue ASTM D-4530-85	
DB Naph	- debutanized naphtha	C5- 221°C
Lt. Naph	- light naphtha	C5- 121°C
Hvy. Naph	- heavy naphtha	121°C - 221°C
LCGO	- light cycle gas oil	221°C - 343°C
HCGO	- heavy cycle gas oil	343°C - 565°C
RON	- research octane number	
B/D	- barrels/day (1 B/D = 159 litres/day)	

Claims

1. A fluid catalytic cracking process comprising:

cracking a hydrocarbon feedstock in suspension with a fluidized catalyst at a catalytic reaction temperature

to form a mixture of cracked hydrocarbon and spent catalyst, and centrifugally separating said mixture in a centrifugal separator into a predominantly cracked hydrocarbon portion and a predominantly spent catalyst portion;

5 characterized by
discharging a quench fluid into said centrifugal separator into said predominantly cracked gas portion but not into said predominantly spent catalyst portion

10 2. A process according to claim 1 characterized by regenerating said spent catalyst at a regeneration temperature above said catalytic reaction temperature to yield regenerated catalyst and passing said regenerated catalyst for use in said cracking step

3. A process according to claim 2 characterized in that said regeneration temperature is in the range of substantially 650°C to 760°C

15 4. A process according to any one of claims 1 to 3 characterized in that said quenching step does not precede said separating step

20 5. A process according to any one of claims 1 to 4 characterized in that said catalytic reaction temperature is in the range of substantially 510°C to 540°C.

6. A process according to any one of claims 1 to 5 characterized in that said unreactive temperature is at least 22°C below said catalytic reaction temperature.

25 7. A process according to claim 6 characterized in that said unreactive temperature is about 22°C to 28°C below said catalytic reaction temperature.

8. Apparatus for the fluid catalytic cracking of a hydrocarbon feedstock comprising:

30 a riser conversion zone defined by a vertically elongate tubular conduit (40) having a lower upstream end and an upper downstream end (49), said downstream end terminating within a reactor vessel (120);
means (20,30) for providing a suspension of hydrocarbon feedstock and catalyst at the upstream end of said riser conversion zone to produce a mixture of spent catalyst and cracked hydrocarbon discharging from the downstream end (49) of said riser conversion zone; and
35 a first conduit (52) directly connecting the downstream end (49) of said riser conversion zone to a separator (50);

characterized in that:

40 said separator (50) comprises:

a curved separation flow channel shaped to cause said mixture to flow therearound including a separation surface (54) on the outside of the curved separation flow channel wherein said mixture is centrifugally separated into a predominantly spent catalytic phase in contact with the separation surface (54) and a predominantly cracked hydrocarbon phase spaced from said surface and on the inside of the curved separation flow channel;

45 and
a second conduit (57) for providing a quench fluid to a nozzle (60) located on the inside of the curved separation flow channel into the cracked hydrocarbon phase and having a discharge pattern causing discharge of substantially all of said quench fluid into said separated cracked hydrocarbon phase.

50

Patentansprüche

1. Fließkatalysator-Crackingverfahren, umfassend:

55 Cracken eines Kohlenwasserstoff-Ausgangsmaterials in Suspension mit einem fluidisierten Katalysator mit einer katalytischen Reaktionstemperatur zur Bildung eines Gemisches aus gecracktem Kohlenwasserstoff und verbrauchtem Katalysator; und
Schleudertrennen des genannten Gemisches in einer Schleudertrennvorrichtung in einen vorwiegend ge-

crackten Kohlenwasserstoffteil und einen vorwiegend verbrauchten Katalysatorteil, gekennzeichnet durch das Einleiten eines Quenchfluids in die genannte Schleudertrennvorrichtung in den genannten, vorwiegend gecrackten Gasteil, aber nicht in den genannten vorwiegend verbrauchten Katalysatorteil

- 5 2. Verfahren nach Anspruch 1, gekennzeichnet durch das Regenerieren des genannten verbrauchten Katalysators mit einer Regenerationstemperatur oberhalb der genannten katalytischen Reaktionstemperatur, um regenerierten Katalysator zu erhalten, und Passieren des genannten regenerierten Katalysators zur Verwendung in dem genannten Cracking-Schritt
- 10 3. Verfahren nach Anspruch 2, dadurch gekennzeichnet, daß die genannte Regenerationstemperatur im Bereich zwischen im wesentlichen 650°C und 760°C liegt.
4. Verfahren nach einem der Ansprüche 1 bis 3, dadurch gekennzeichnet, daß der genannte Quenchschritt nicht vor dem genannten Trennschritt durchgeführt wird
- 15 5. Verfahren nach einem der Ansprüche 1 bis 4, dadurch gekennzeichnet, daß die genannte katalytische Reaktionstemperatur im Bereich zwischen im wesentlichen 510°C und 540°C liegt
6. Verfahren nach einem der Ansprüche 1 bis 5, dadurch gekennzeichnet, daß die genannte unreaktive Temperatur wenigstens 22°C unterhalb der genannten katalytischen Reaktionstemperatur liegt.
- 20 7. Verfahren nach Anspruch 6, dadurch gekennzeichnet, daß die genannte unreaktive Temperatur etwa 22°C bis 28°C unter der genannten katalytischen Reaktionstemperatur liegt.
- 25 8. Vorrichtung zum fließkatalytischen Cracken eines Kohlenwasserstoff-Ausgangsmaterials, umfassend:

eine Riser-Konvertierungszone, definiert durch einen vertikal länglichen röhrenförmigen Kanal (40) mit einem unteren aufwärtigen Ende und einem oberen abwärtigen Ende (49), wobei das genannte abwärtige Ende in einem Reaktorbehälter (120) endet;

Mittel (20, 30) zum Bereitstellen einer Suspension aus Kohlenwasserstoff-Ausgangsmaterial und Katalysator am aufwärtigen Ende der genannten Riser-Konvertierungszone zum Erzeugen eines Gemisches aus verbrauchtem Katalysator und gecracktem Kohlenwasserstoff, der aus dem abwärtigen Ende (49) der genannten Riser-Konvertierungszone abläuft; und

einen ersten Kanal (52), der das abwärtige Ende (49) der genannten Riser-Konvertierungszone zu einem Abscheider (50) unmittelbar verbindet;

dadurch gekennzeichnet, daß der genannte Abscheider (50) folgendes umfaßt:

einen gekrümmten Trennströmungskanal, der so geformt ist, daß er bewirkt, daß das genannte Gemisch um ihn herumfließt, einschließlich einer Trennfläche (54) an der Außenseite des gekrümmten Trennströmungskanals, worin das genannte Gemisch in eine vorwiegend verbrauchte katalytische Phase in Kontakt mit der Trennoberfläche (54) und eine vorwiegend gecrackte Kohlenwasserstoffphase schleudertrennt wird, die von der genannten Oberfläche beabstandet ist und an der Innenseite des gekrümmten Trennströmungskanals liegt; und

einen zweiten Kanal (57) zum Zuführen eines Quenchfluids zu einer Düse (60), die sich an der Innenseite des gekrümmten Trennströmungskanals in die gecrackte Kohlenwasserstoffphase befindet und die einen Ablaufkonus hat, der einen Ablauf von im wesentlichen dem gesamten genannten Quenchfluid in die genannte getrennte, gecrackte Kohlenwasserstoffphase bewirkt.

Revendications

1. Procédé de craquage catalytique de fluide comprenant :

le craquage d'une charge d'hydrocarbures en suspension avec un catalyseur fluidisé à une température de réaction catalytique afin de former un mélange d'hydrocarbures craqués et de catalyseur usé ; et la séparation dudit mélange par centrifugation dans un séparateur centrifuge en une partie contenant principalement les hydrocarbures craqués et une partie contenant principalement le catalyseur usé ;

caractérisé par le fait de décharger un fluide d'extinction dans ledit séparateur centrifuge dans ladite partie contenant principalement les gaz craqués mais non dans ladite partie contenant principalement le catalyseur usé

- 5 2. Procédé selon la revendication 1, caractérisé par le fait de régénérer ledit catalyseur usé à une température de régénération supérieure à ladite température de réaction catalytique afin de produire un catalyseur régénéré, et de passer ledit catalyseur régénéré afin de l'utiliser dans ladite étape de craquage
- 10 3. Procédé selon la revendication 2, caractérisé en ce que ladite température de régénération est comprise sensiblement entre 650° et 760°C
4. Procédé selon l'une quelconque des revendications 1 à 3, caractérisé en ce que ladite étape d'extinction ne précède pas ladite étape de séparation
- 15 5. Procédé selon l'une quelconque des revendications 1 à 4, caractérisé en ce que ladite température de réaction catalytique est comprise sensiblement entre 510°C et 540°C
6. Procédé selon l'une quelconque des revendications 1 à 5, caractérisé en ce que ladite température non réactive est au moins de 22°C inférieure à ladite température de réaction catalytique.
- 20 7. Procédé selon la revendication 6, caractérisé en ce que ladite température non réactive est environ de 22°C à 28°C inférieure à ladite température de réaction catalytique.

- 25 8. Appareil pour le craquage catalytique de fluide d'une charge d'hydrocarbures comprenant :

une zone de conversion en colonne montante définie par un conduit tubulaire s'étendant verticalement (40) ayant une extrémité amont inférieure et une extrémité aval supérieure (49), ladite extrémité aval débouchant dans une cuve de réaction (120) ;

des moyens (20, 30) pour délivrer une suspension de charge d'hydrocarbures et de catalyseur à l'extrémité amont de ladite zone de conversion en colonne montante afin de produire un mélange de catalyseur usé et d'hydrocarbures craqués déchargé à l'extrémité aval (49) de ladite zone de conversion en colonne montante ; et

un premier conduit (52) connectant directement l'extrémité aval (49) de ladite zone de conversion en colonne montante à un séparateur (50) ;

caractérisé en ce que :

ledit séparateur (50) comprend :

un canal d'écoulement de séparation coudé profilé de manière à provoquer l'écoulement du mélange dans celui-ci, comprenant une surface de séparation (54) à l'extérieur du canal d'écoulement de séparation coudé, où ledit mélange est séparé par centrifugation en une phase contenant principalement du catalyseur usé en contact avec la surface de séparation (54) et une phase contenant principalement des hydrocarbures craqués espacée de ladite surface et sur l'intérieur du canal d'écoulement de séparation coudé ; et

un deuxième conduit (57) pour délivrer un fluide d'extinction à une buse (60) située à l'intérieur du canal d'écoulement de séparation coudé dans la phase d'hydrocarbures craqués et ayant un motif de décharge provoquant la décharge de sensiblement tout ledit fluide d'extinction dans ladite phase d'hydrocarbures craqués séparée.

FIG. 1.

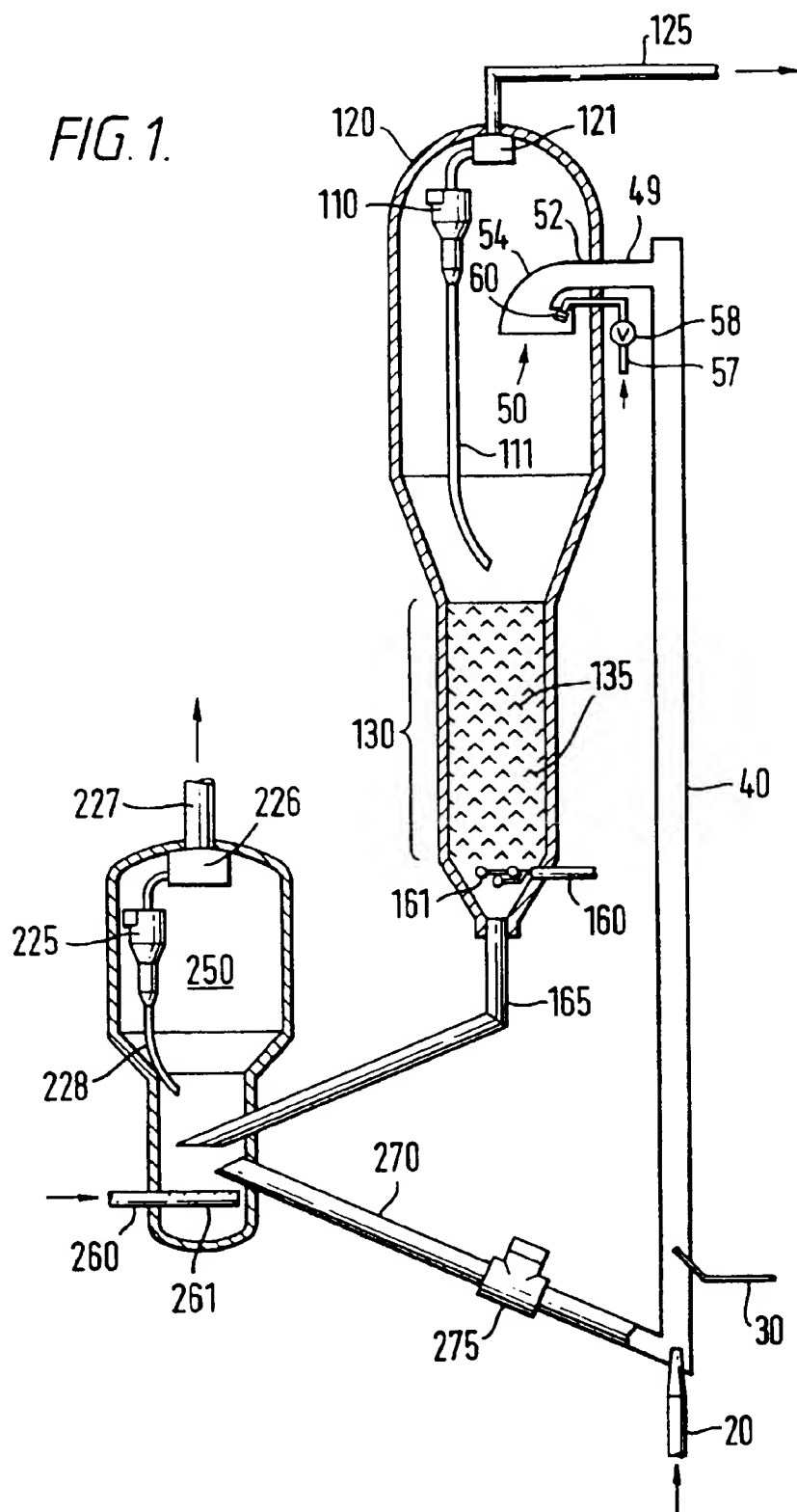


FIG. 2.

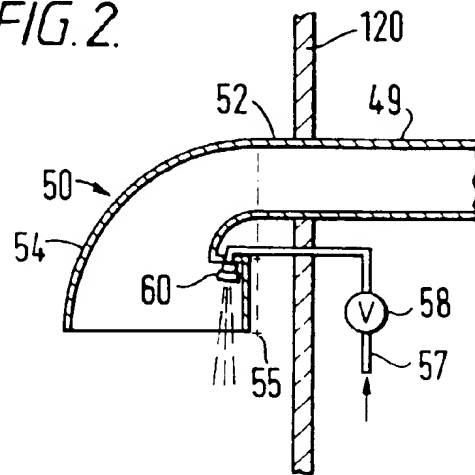


FIG. 3A

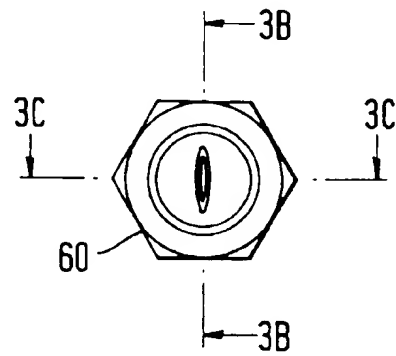


FIG. 3B

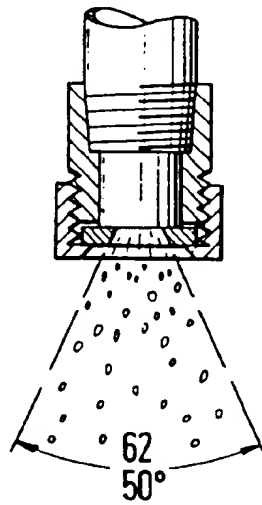


FIG. 3C

